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DESCRIPTION**Wavelength-Variable Light Outputting Apparatus****Technical Field**

The present invention relates to a wavelength-variable
5 light outputting apparatus for irradiating an object with
light whose wavelength is made variable.

Background Art

A conventional wavelength-variable light outputting
apparatus is disclosed in Japanese Patent Application
10 Laid-Open No. HEI 1-223929. In this apparatus, light
outputted from a light source is made incident on an optical
filter rotator having three colors of red (R), green (G),
and blue (B), whereby light having a desirable wavelength
is outputted therefrom. For controlling color light
15 quantities independently from each other, it will be
sufficient if a plurality of liquid crystal filters, ND
filters having respective light attenuation ratios different
from each other, and the like are arranged on the output
side of each optical filter and switched therebetween.

20 Disclosure of the Invention

The conventional wavelength-variable light outputting
apparatus can be used for observing biological samples.
Namely, when a fluorescence-labeled biological sample
disposed under a microscope is irradiated with monochromatic
25 light having a selected wavelength as pumping light,
fluorescence occurs from the biological sample. Thus

generated fluorescence can be captured as a fluorescent image of the biological sample.

Since the transmission or absorption wavelength band of a material constituting the sample varies depending on
5 the kind of material, a sample image reflecting the material constituting the sample can be obtained if the sample image is captured with variable wavelengths.

Since a plurality of wavelengths of light are necessary depending on kinds of fluorescence labels and
10 sample-constituting materials, it is desirable that wavelengths be rapidly changed and switched in order to shorten the measurement time. When combining images obtained upon irradiation with a plurality of wavelengths, in particular, it is preferred that the irradiation light
15 quantity be constant from the viewpoint of utility in analysis.

However, wavelength sweeping cannot be carried out at a high speed in the above-mentioned conventional apparatus. Namely, the light from the light source has a wavelength
20 distribution, so that its light quantity differs from wavelength to wavelength, whereby it is necessary for a plurality of optical filters and ND filters provided independently from each other to rotate and move at a high speed in order to make wavelengths variable while maintaining
25 a constant light quantity. However, continuous wavelength sweeping requires a number of filters, each of which has

a large mass, so that a driving apparatus moving such a structure while controlling its position can operate only at a relatively low speed.

In view of the problem mentioned above, it is an object
5 of the present invention to provide a wavelength-variable light outputting apparatus which can make wavelengths variable at a high speed while controlling light quantities.

For overcoming the above-mentioned problem, the present invention provides a wavelength-variable light
10 outputting apparatus comprising a light source outputting light having a plurality of wavelengths, a swinging first galvanometric scanner provided with spectroscopic means for spectrally dividing the light outputted from the light source, a swinging second galvanometric scanner provided with a
15 shielding or reflecting member adapted to block or reflect at least a part of light outputted from the spectroscopic means, and an optical fiber disposed at a position where light outputted from the spectroscopic means can be made incident by way of the shielding or reflecting member.

20 The light outputted from the light source is fed into spectroscopic means such as a diffraction grating or prism. Since the spectroscopic means spectrally divides the light outputted from the light source, the emitting direction of a specific wavelength component among thus divided light
25 components can be deflected by swinging the first galvanometric scanner. This specific wavelength component

is made incident on the shielding or reflecting member, whereby a part thereof is blocked or reflected. Since such a member is provided with the second galvanometric scanner, the transmission light quantity or reflecting direction of
5 the specific wavelength component varies when the second galvanometric scanner is swung.

Since the optical fiber is disposed at a position where light outputted from the spectroscopic means can be made incident by way of the shielding or reflecting member, the
10 quantity of light finally incident on the optical fiber can vary if the transmission light quantity is made variable by the shielding member, whereas, due to the fact that the input end face of the optical fiber has a core with a finite diameter, the quantity of light finally entering the core
15 of the optical fiber will vary if the reflecting direction is made variable by the reflecting member.

Thus, since galvanometric scanners which can swing at a high speed are provided with the spectroscopic means and the shielding or reflecting member, this wavelength-variable
20 light outputting apparatus can select a specific wavelength component at a high speed and make its light quantity variable at a high speed.

Preferably, this wavelength-variable light outputting apparatus comprises storage means for storing respective
25 swinging angles of the first and second galvanometric scanners and a relationship between the wavelength and

quantity of light outputted from the optical fiber in response to a combination of the swinging angles, input means for inputting information concerning the wavelength and quantity of light to be outputted from the optical fiber, and control
5 means for reading out the above-mentioned relationship from the storage means according to the information fed into the input means and controlling the swinging angles of the first and second galvanometric scanners in response to the relationship.

10 The storage means such as a memory stores therein respective swinging angles of the first and second galvanometric scanners and a relationship between the wavelength and quantity of light outputted from the optical fiber in response to a combination of the swinging angles.
15 When information concerning the wavelength and quantity of light to be outputted from the optical fiber is fed into the input means such as a keyboard, the control means reads out the above-mentioned relationship from the storage means according to the information fed into the input means, and
20 controls the swinging angles in response to this relationship. Namely, the wavelength and quantity of light outputted from the optical fiber can definitely be determined according to a combination of swinging angles, whereby desirable light can be outputted from the optical fiber based on the input
25 to the input means alone.

Also, this wavelength-variable light outputting

apparatus may comprise control means for changing the wavelength of light outputted from the optical fiber by changing a swinging angle of the first galvanometric scanner and changing a swinging angle of the second galvanometric scanner such that the quantity of the wavelength of light fed to the shielding or reflecting member in response to the swinging angle of the first galvanometric scanner and the ratio of incidence of light incident on the optical fiber in response to the swinging angle of the second galvanometric scanner form a fixed product therebetween.

When the swinging angle of the first galvanometric scanner is changed, the wavelength of light outputted from the optical fiber changes. The quantity of the wavelength of light fed to the shielding or reflecting member varies depending on this swinging angle. In order for the light finally outputted from the optical fiber to become constant, it will be sufficient if the quantity of the wavelength of light fed to the shielding or reflecting member in response to the swinging angle of the first galvanometric scanner and the ratio of incidence of the light incident on the optical fiber in response to the swinging angle of the second galvanometric scanner form a fixed product therebetween.

The control means changes the swinging angle of the second galvanometric scanner so as to satisfy this relationship. If the swinging angle of the second galvanometric scanner for satisfying such a relationship

is determined beforehand by use of a calculation or lookup table system, the time required for determining it can be shortened, whereby the wavelength can be made variable at a higher speed under a constant light quantity. However, 5 the swinging angle of the second galvanometric scanner may also be determined sequentially in response to the swinging angle of the first galvanometric scanner.

Brief Description of the Drawings

Fig. 1 is an explanatory view showing the configuration 10 of a wavelength-variable light outputting apparatus;

Figs. 2A, 2B, and 2C are explanatory views showing relationships between positions of a shielding member 11 and light incident on an optical fiber 10;

Fig. 3 is a block diagram showing a system configuration 15 of a fluorescent image capturing apparatus using the above-mentioned wavelength-variable light outputting apparatus;

Fig. 4 is an explanatory view showing the configuration of the wavelength-variable light outputting apparatus in 20 accordance with another embodiment;

Figs. 5A, 5B, and 5C are explanatory views showing positional relationships between the input end face (core) F of the optical fiber 10 and a light-collecting spot S;

Fig. 6 is a graph showing the change in quantity 25 (intensity) of light outputted from the optical fiber 10 with time when light incidence ratio β was changed from 100%

to 50%; and

Fig. 7 is a graph showing the change in quantity (intensity) of light outputted from the optical fiber 10 with time when light incidence ratio β was changed from 100% to 0%.

Best Modes for Carrying Out the Invention

In the following, wavelength-variable light outputting apparatus in accordance with embodiments will be explained. In the explanation, constituents identical to each other will be referred to with numerals identical to each other without repeating their overlapping descriptions.

Fig. 1 is an explanatory view showing the configuration of a wavelength-variable light outputting apparatus. This wavelength-variable light outputting apparatus is constituted by a light source section 100 for emitting light, and a spectroscopic section 101 for spectrally dividing the emitted light while adjusting the light quantity thereof. This will be explained in more detail.

The wavelength-variable light outputting apparatus comprises a light source 1 such as an Xe lamp. Though the light outputted from the light source 1 diverges in all directions, it is reflected to the front side of the light source 1 by a small concave reflecting mirror 2 disposed so as to face the light source 1 on the back side (left side in the drawing) thereof, and is made incident on a large

concave reflecting mirror 4 by way of a lens 3 together with the light directly emitted from the light source 1 to the front side.

A convex reflecting mirror 5 is disposed near the center of curvature of the concave reflecting mirror 4, so that the light reflected by the concave reflecting mirror 4 is reflected again toward the concave reflecting mirror 4. The light reflected twice by the concave reflecting mirror 4 is converged at a position where an entrance slit 6 is disposed, and passes through the slit 6. The light emitted from the slit 6 is collimated by an off-axis parabolic mirror 7, so as to irradiate a diffraction grating (spectroscopic means) 8 which is rotatably movable.

The light irradiated on the diffraction grating 8 is spectrally divided into separate wavelength components which are made incident on the off-axis parabolic mirror 9, and are converged thereby onto an input end face of an optical fiber 10. A rotatably movable shielding member 11 is disposed in an optical path between the off-axis parabolic mirror 9 and the optical fiber 10. The light converged onto the input end face of the optical fiber 10 passes through the optical fiber 10, so as to be outputted from the output end face thereof.

The diffraction grating 8 is attached to a first galvanometric scanner 12, whereas the first galvanometric scanner 12 swings the diffraction grating 8 while using an

axis perpendicular to the optical axis of light incident on the diffraction grating 8 as the axis of swinging. When the diffraction grating 8 is swung by driving the first galvanometric scanner 12, the advancing direction of a
5 specific wavelength component outputted from the diffraction grating 8 is deflected, whereby the light fed to the optical fiber 10 changes its wavelength.

The light-shielding member 11 disposed in the optical path leading to the optical fiber 10 is attached to a second
10 galvanometric scanner 13, which swings the light-shielding member 11 while using an axis perpendicular to the optical axis of light incident on the optical fiber 10 as the axis of swinging. When the second galvanometric scanner 13 is driven so as to swing the light-shielding member 11, the
15 light incident on the optical fiber 10 is partly blocked by the shielding member 11, whereby the quantity of light fed into the optical fiber 10 changes.

Figs. 2A, 2B, and 2C are explanatory views showing relationships between positions of the shielding member 11 and light incident on the optical fiber 10. As shown in these
20 drawings, the swinging axis of the second galvanometric scanner 13 does not intersect the optical axis of the optical fiber 10, but is positioned outside the effective diameter, perpendicular to the optical axis, of the light converged
25 onto the input end face of the optical fiber 10.

When the whole light-shielding member 11 is positioned

outside the convergent light as shown in Fig. 2A, 100% of the convergent light enters the optical fiber 10 (incidence ratio $\beta = 100\%$).

When an outer edge of the light-shielding member 11
5 on the optical axis side is positioned on the optical axis of the convergent light as shown in Fig. 2B, 50% of the convergent light enters the optical fiber 10 (incidence ratio $\beta = 50\%$).

When the whole light-shielding member 11 is positioned
10 within the optical path of the convergent light as shown in Fig. 2C, 0% of the convergent light enters the optical fiber 10 (incidence ratio $\beta = 0\%$).

Thus, the swinging angle θ_2 of the light-shielding member 11 and the incidence ratio β of convergent light
15 correspond to each other one to one. Similarly, the swinging angle θ_1 of the diffraction grating 8 and the emission angle of output light from the diffraction grating 8, i.e., the advancing direction of a specific wavelength component, correspond to each other one to one. The diffraction grating
20 8 can be replaced by a prism which spectrally divides light in a similar fashion.

Fig. 3 is a block diagram showing a system configuration of a fluorescent image capturing apparatus using the above-mentioned wavelength-variable light outputting
25 apparatus. This fluorescent image capturing apparatus combines the wavelength-variable light outputting apparatus

with an imaging device 14. Namely, in this apparatus, a fluorescence-labeled biological sample SM is irradiated with light emitted from the optical fiber 10, and a fluorescent image of the sample generated upon the irradiation is captured
 5 by the imaging device 14.

This diagram shows a control unit (control means) 15 for controlling the light source 1 and scanners 12, 13 in the wavelength-variable light outputting apparatus; a storage device (storage means) 16 such as a memory for storing
 10 control conditions effected by the control unit 15, an input device (input means) 17 such as a keyboard with which an operator inputs operations of the wavelength-variable light outputting apparatus, and a display 18 for displaying the information about input to the input device 17 and the image
 15 captured by the imaging device 14.

The storage device 16 in this apparatus stores the respective swinging angles θ_1 , θ_2 of the first and second galvanometric scanners 12, 13 and the relationship $((\theta_1, \theta_2) = (\lambda, E))$ between the wavelength λ and quantity E of
 20 light outputted from the optical fiber 10 in response to the combination of the swinging angles θ_1 , θ_2 . Here, the wavelength refers to the center wavelength.

Information (λ, E) concerning the wavelength λ and quantity E of light to be outputted from the optical fiber
 25 10 is fed into the input device 17.

According to the information (λ, E) fed into the input

device 17, the control unit 15 reads out the relationship
 $((\lambda, E) = (\theta_1, \theta_2))$ from the storage device 16, and controls
the swinging angles θ_1, θ_2 of the first and second
galvanometric scanners 12, 13 in conformity to this
5 relationship. Namely, (θ_1, θ_2) is determined so as to match
target (λ, E) , and the first and second galvanometric scanners
12, 13 are driven so as to attain (θ_1, θ_2) . Thereafter, the
control unit 15 turns on the light source 1 or carries out
the driving while turning on the light source 1.

10 Namely, this apparatus can definitely determine the
wavelength λ and quantity E of light to be outputted from
the optical fiber 10 according to the combination of swinging
angles (θ_1, θ_2) , thereby being able to output desirable light
from the optical fiber 10 in response to the input to the
15 input device 17 alone.

The following table shows the center wavelength (nm)
and half width (nm) of light emitted from the optical fiber
10 in the case where the quantity of light (output) (mW)
is made variable at each of wavelengths λ of 380 nm, 500
20 nm, and 650 nm.

$\lambda=380$ nm			$\lambda=500$ nm			$\lambda=650$ nm		
output (mW)	center wavelength (nm)	half width	output (mW)	center wavelength (nm)	half width	output (mW)	center wavelength (nm)	half width
2.88	380.1	15.5	3.32	500.2	14.4	1.25	650.0	13.7
2.61	380.1	15.4	3.00	500.2	14.6	1.12	650.0	13.7
2.32	380.1	15.6	2.67	500.2	14.7	1.00	650.0	13.7
2.02	380.1	15.5	2.32	500.2	14.5	0.88	650.0	13.7
1.74	380.1	15.5	1.98	500.2	14.6	0.75	650.0	13.7
1.43	380.1	15.5	1.65	500.2	14.3	0.62	650.0	13.5
1.16	380.1	15.2	1.32	500.2	14.3	0.50	650.0	13.5
0.87	380.1	15.1	1.00	500.2	14.1	0.37	650.0	13.0
0.57	380.1	15.0	0.66	500.7	13.8	0.25	650.0	12.5
0.25	380.1	14.3	0.29	501.2	13.1	0.11	650.0	11.7

As can be seen from this table, it is verified in this apparatus that changes in light quantity do not alter the center wavelength, and hardly vary the half width.

While altering the output light wavelength λ from the
 5 optical fiber 10 by changing the swinging angle θ_1 of the
 first galvanometric scanner 12, the swinging angle θ_2 of
 the second galvanometric scanner 13 may be changed such that
 the product of the light quantity e of the wavelength of
 light fed to the shielding member 11 or a reflecting member
 10 11', which will be explained later, in response to the swinging
 angle θ_1 , and the ratio of incidence β of light incident
 on the optical fiber 10 in response to the swinging angle
 θ_2 of the second optical fiber 10, $(e \times \beta) = E$, becomes constant.

When the swinging angle θ_1 of the first galvanometric
 15 scanner 12 is altered, the output light wavelength λ from
 the optical fiber 10 changes. Since the light emitted from
 the light source 1 has a wavelength distribution, the light
 quantity e of the wavelength of light fed to the shielding
 or reflecting member 11, 11' in response to the swinging
 20 angle θ_1 varies. For making the quantity E of light finally
 outputted from the optical fiber 10 constant, it will be
 sufficient if the light quantity e of the wavelength of light
 fed to the shielding or reflecting member 11, 11' in response
 to the swinging angle θ_1 of the first galvanometric scanner
 25 12, and the incidence ratio β of the light incident on the
 optical fiber 10 in response to the swinging angle θ_2 of

the second galvanometric scanner 13 form a fixed product therebetween.

The control unit 15 changes the swinging angle θ_2 of the second galvanometric scanner 13 so as to satisfy the above-mentioned relationship. If the swinging angle θ_2 of the second galvanometric scanner 13 for satisfying such a relationship is determined beforehand by use of a calculation or lookup table system, the time required for determining it can be shortened, whereby the wavelength can be made variable at a higher speed under a constant light quantity. However, the swinging angle θ_2 of the second galvanometric scanner 13 can be determined sequentially in response to the swinging angle θ_1 of the first galvanometric scanner 12.

Finally, the light quantity control using the reflecting member 11' will be explained.

Fig. 4 is an explanatory view showing the configuration of the wavelength-variable light outputting apparatus in accordance with another embodiment. This apparatus differs from that of the above-mentioned one only in that the member provided in the second galvanometric scanner 2 is not the shielding member 11 but the reflecting member 11', and that the swinging axis of the second galvanometric scanner 13 is disposed oblique with respect to the optical axis of light incident on the reflecting member 11'.

Namely, a specific wavelength component in the light

spectrally divided by the diffraction grating 8 is converged by an off-axis parabolic mirror 9, and is reflected by the reflecting member 11' disposed in the optical path between the off-axis parabolic mirror 9 and the optical fiber 10, so as to be converged onto the input end face F of the optical fiber 10 (S being a spot of converged light). Therefore, due to the swinging of the second galvanometric scanner 13, the position of light-collecting spot S moves, whereby the light incidence ratio β to the optical fiber changes.

10 Figs. 5A, 5B, and 5C are explanatory views showing positional relationships between the input end face (core) F of the optical fiber 10 and the light-collecting spot S.

When the position of converged light spot S and the position of optical fiber end face F coincide with each other, i.e., their centers of gravity coincide with each other, so that the spot S and the end face F completely overlay each other as shown in Fig. 5A, the light incidence ratio β is 100%.

When the position of converged light spot S and the position of optical fiber end face F slightly deviate from each other, i.e., their centers of gravity shift from each other, so that the spot S and end face F partly overlap each other as shown in Figs. 5B and 5C, the light incidence ratio β is greater than 0% but smaller than 100%. When no overlap exists, the light incidence ratio β is 0%.

Thus, in this embodiment, the second galvanometric

scanner 13 is driven so as to swing the reflecting member 11', whereby the light incidence ratio β can be changed.

The quantity of light outputted from the optical fiber 10 in the wavelength-variable light outputting apparatus in the former embodiment was measured at a wavelength of 380 nm. Here, for verifying whether high-speed variation was possible or not, the light incidence ratio β was changed by driving the second galvanometric scanner 13.

Fig. 6 is a graph showing the change in quantity (intensity) of light outputted from the optical fiber 10 with time when the light incidence ratio β was changed from 100% to 50%.

Fig. 7 is a graph showing the change in quantity (intensity) of light outputted from the optical fiber 10 with time when the light incidence ratio β was changed from 100% to 0%. These light quantities were detected by a photodiode.

In both graphs, signals in the upper half indicate the quantity of light (2 V/div), whereas signals in the lower half indicate driving signals fed into the second galvanometric scanner 13 (5 V/div), with a temporal axis of 2 ms/div. These graphs have proved that changes in light quantity can be completed in a short time of 2 ms or less after the application of driving signals in both cases.

The above-mentioned wavelength-variable light outputting apparatus can be applied not only to the

fluorescent image capturing apparatus, but also to a transmitted or absorbed light image capturing apparatus for yielding a sample image reflecting a sample-constituting material if the sample image is captured at variable
5 wavelengths. The images obtained at these plurality of wavelengths can be combined by the control unit 15 shown in Fig. 3, so as to be displayed on the display 18.

As explained in the foregoing, the above-mentioned wavelength-variable light outputting apparatus comprises
10 the light source 1 outputting light having a plurality of wavelengths, the swinging first galvanometric scanner 12 provided with the spectroscopic means 8 for spectrally dividing the light outputted from the light source 1, the swinging second galvanometric scanner 13 provided with the
15 shielding member 11 or reflecting member 11' adapted to block or reflect at least a part of light outputted from the spectroscopic means 8, and the optical fiber 10 disposed at a position where light outputted from the spectroscopic means 8 can be made incident by way of the shielding or
20 reflecting member 11, 11'.

The light outputted from the light source 1 is fed into spectroscopic means 8 such as a diffraction grating or prism. Since the spectroscopic means 8 spectrally divides the light outputted from the light source 1, the emitting direction
25 of a specific wavelength component among thus divided light components can be deflected by swinging the first

galvanometric scanner 12. This specific wavelength component is made incident on the shielding member 11 or reflecting member 11', whereby a part thereof is blocked or reflected. Since such a member is provided with the second
5 galvanometric scanner 13, the transmission light quantity or reflecting direction of the specific wavelength component is variable when the second galvanometric scanner 13 is swung.

Since the optical fiber 10 is disposed at a position where light outputted from the spectroscopic means 8 can
10 be made incident by way of the shielding or reflecting member 11, 11', the quantity of light finally incident on the optical fiber 10 can vary if the transmission light quantity is made variable by the shielding member 11 whereas, due to the fact that the input end face F of the optical fiber 10 has a core
15 with a finite diameter, the quantity of light finally entering the core of the optical fiber 10 will vary if the reflecting direction is made variable by the reflecting member 11'.

Thus, since the galvanometric scanners 12, 13, which can swing at a high speed are provided with the spectroscopic
20 means 8 and the shielding or reflecting member 11, 11', respectively, the above-mentioned wavelength-variable light outputting apparatus can select a specific wavelength component at a high speed and make its light quantity variable at a high speed. As mentioned above, such an apparatus is
25 useful for capturing a fluorescent image of the biological sample SM. By way of the shielding member 11, light is made

incident on the optical fiber 10 and is outputted therefrom,
whereby the biological sample SM can effectively be
irradiated with light.

The present invention can provide a
5 wavelength-variable light outputting apparatus which can
make wavelengths variable at a high speed while controlling
light quantities.

Industrial Applicability

The present invention can be utilized in a
10 wavelength-variable light outputting apparatus for
irradiating an object with light whose wavelength is made
variable.